

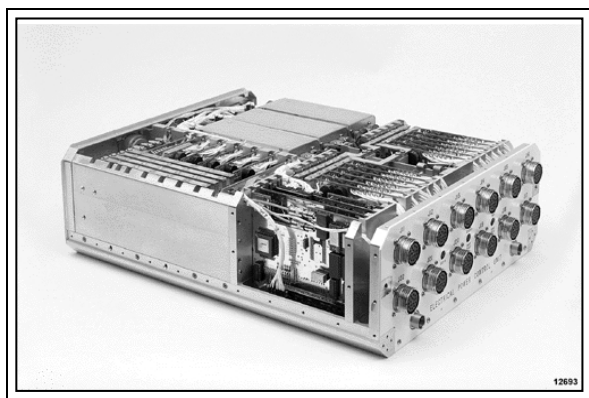
Testing of the Engineering Model Electrical Power Control Unit for the Fluids and Combustion Facility

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ABSTRACT

The *John H. Glenn Research Center at Lewis Field* (GRC) in Cleveland, OH and the Sundstrand Corporation in Rockford, IL have designed and developed an *Engineering Model* (EM) *Electrical Power Control Unit* (EPCU) for the *Fluids Combustion Facility* (FCF) experiments to be flown on the *International Space Station* (ISS). The EPCU will be used as the power interface to the ISS power distribution system for the FCF's space experiments' test and telemetry hardware. Furthermore, it is proposed to be the common power interface for all experiments.



EM EPCU with Cover Removed
Photograph 1

The EPCU is a three kilowatt 120Vdc-to-28Vdc converter utilizing three independent *Power Converter Units* (PCUs), each rated at 1kWe (36Adc @ 28Vdc) which are paralleled and synchronized. Each converter may be fed from one of two ISS power channels. The 28Vdc loads are connected to the EPCU output via 48 solid-state and current-limiting switches, rated at 4Adc each. These switches may be paralleled to supply any given load up to the 108Adc normal operational limit of the paralleled converters. The EPCU was designed in this manner to maximize allocated-power utilization, to shed loads autonomously, to provide fault tolerance, and to provide a flexible power converter and control module to meet various ISS load demands.

Tests of the EPCU in the Power Systems Facility tested at GRC reveal that the overall converted-power efficiency is approximately 89%--with a nominal-input voltage of 120Vdc and a total load in the range of 40% to

110% rated 28Vdc load. (The PCUs alone have an efficiency of approximately 94.5%.) Furthermore, the EM unit passed all flight-qualification level (and beyond) vibration tests, passed ISS EMI (conducted, radiated, and susceptibility) requirements, successfully operated for extended periods in a thermal/vacuum chamber, was integrated with a proto-flight experiment, and passed all stability and functional requirements.

Due to paper length limitations, this Technical Memorandum only overviews EPCU operation and tests; a more detailed test report is available [1], as is a Technical Memorandum explaining operational details [2].

INTRODUCTION & OPERATIONAL OVERVIEW

The EPCU is an ISS power interface, which converts 120Vdc to 28Vdc, and was designed for the FCF experiments. The rated, converted power is 3kWe @ 28Vdc and is available via 48 4Adc output-channels (4 channels per connector) on the front of the unit. Furthermore, the EPCU provides an additional 2.9kWe of unprocessed—but protected—power at 120Vdc. These 120Vdc feed-throughs are contained in groups of three per connector (two connectors) on the back of the EPCU. The EPCU's feed-through power is not processed: these load connectors are fed by *DC-to-DC Converter Units* (DDCUs) and are subject to DDCU power quality.

Power protection is accomplished with current limiting, solid-state switches which trip according to a v^2t timing. (The switch FET voltage is controlled to achieve the current-limiting value of 4Adc: as the load current increases, the voltage drop across the FET increases. The hybrid trips more quickly as the connected load increases beyond the current-limiting value.) These solid-state switches, along with the control and monitoring hardware, are called *Remote Power Controllers* (RPCs) and have been packaged into a hybrid module. These hybrid switches, which can operate at voltage levels from 18Vdc to 150Vdc, are the keys to the flexibility and re-configurability of the EPCU.

Because the RPC channels can operate individually or be paralleled in groups of two, three, or four RPCs (i.e., channel capacities of 4Adc, 8Adc, 12Adc, or 16Adc), the EPCU can readily feed any variety of user loads

requiring 28Vdc simply by swapping-out external loads' harnesses, which are connected at the front of the EPCU (see Photograph 1). By selecting a harness, which parallels the required number of channels, the EPCU eliminates the need for "experiment-specific" power interfaces. (The harnesses contain programming pins, which cause paralleled channels to operate as if they were one.)

One of the most significant design features of the EPCU is its autonomous power-limiting design, which efficiently utilizes ISS power, and ensures that the EPCU autonomously limits the connected power drawn from the ISS power system. This is accomplished with *Dynamic Power Sharing* (DPS) and *Prioritized Load Shedding* (PLS).

The EPCU has two 120Vdc input feeds which may be connected to either of two independent ISS power channels, and each of the three 1kWe PCUs within the EPCU can be connected to either input feed with a 3PDT relay. The maximum power allocation for each ISS power channel is downloaded to the EPCU via its MIL-STD-1553B interface. (The power allocation needs to be sent only once per the load demand schedule period and does not require that a higher level controller monitor the EPCU.) During normal operation, the EPCU output-paralleled PCUs (inputs are not paralleled!) share output-power equally: as a result, the ISS power feeds proportionally supply the load demand.

This proportional sharing of load, via the DPS controls, continues with increasing load demand until one of the ISS feeds reaches its allocation limit. If the load continues to increase, the PCU(s) connected to the other feed pick up the excess load. This adjustment continues until that feed reaches its allocation limit, at which point the PLS controller begins to shed loads in a prioritized fashion (there are 16 user-selectable levels of priority). Load shedding continues until the busses are again within the allocation limits.

It should be noted that the DPS and PLS functions play a more pivotal role during abnormal operation of the ISS power system. These functions allow the EPCU to continue to feed as much load (i.e., high priority level) as possible in the event that a DDCU feed is lost, severe DDCU voltage droop occurs, other ISS load demand perturbations occur, an EPCU converter fails, or other events which limit the total load capability of the EPCU.

Finally, the EM unit dimensions are approximately 17.5"W x 21.8"D x 6.6"H, and has a mass of approximately 108lbsm. The chassis is a milled aluminum base-plate with aluminum, vertical milled-guides. The three PCUs are mounted directly on the base-plate; whereas all other assemblies (for example, 1553B card) are wedge-locked into place in the guides.

INITIAL FUNCTIONAL TESTS

Prior to performing any higher level tests, basic functional checkouts were performed. These tests included functional verification of the MIL-STD-1553B

interface, RPC isolation and voltage drop characterization, 120Vdc feeder isolation verification, and programming pin and initial position tests.

MIL-STD-1553B INTERFACE CHECKOUT

The 1553B interface was checked to verify that the unit received and implemented basic commands (e.g., bus relay transfer and PCU on/off) and returned proper status information to the software control interface. Accuracy of the sensors and A/D conversion has not yet been quantified.

ISOLATION TESTS

Isolation tests were done on the 120Vdc input channels and on the RPCs (120Vdc and 28Vdc). The input channel isolation tests were done to verify that the ISS input feeds would never be shorted together (it is an ISS requirement that channels never be cross-tied, and this is guaranteed by the break-before-make 3PDT relays) and that the two ISS "hot" and "return" lines were isolated from the EPCU chassis. These are, in fact, the results of the tests.

Isolation of 28Vdc loads connected to the output RPCs (called "A5"s) and 120Vdc loads connected to 120Vdc feed-through RPCs (called "A12"s) were quantified. This was done by turning "off" the A5 and A12 RPCs, applying 120Vdc to the EPCU inputs, turning "on" the converters to energize the *Point of Regulation* (POR) at 28Vdc, and by measuring the output voltage and current of each RPC. The multi-meter provided the short-circuit load for leakage current measurements. Typical A5 leakage was 0.15Vdc @14 μ Adc, and A12 leakage was 2.8Vdc @60 μ Adc.

RPC VOLTAGE DROP TESTS

The test setup had one PCU connected to one power supply ("bus A") and two PCUs to another ("bus B"). Bus A was energized at 120Vdc, and bus B was not energized. The voltage drop across the 28Vdc and 120Vdc RPCs were determined. The A5 channel drop was measured by measuring the POR voltage and the load voltage at half load (2Adc) and full load (4Adc). The difference yields the channel drop. The channel drop was also measured directly and compared with the difference between the POR and load voltage values. Furthermore, because there are 48 4Adc channels and all hybrids were of the same batch, it was decided to only check four 28Vdc channels. The results for the 28Vdc tests are given in Table 1.

The channel-voltage drop at 2Adc is approximately 0.19Vdc, which is an 0.4We loss. At 4Adc the drop is approximately 0.4Vdc, which is a 1.7We loss. These losses correspond to 0.7% and 1.5%, respectively, on a per-channel basis.

Similarly, the 120V_{dc} hybrids were tested, and at 2Adc load the drop across the channel is approximately 0.14Vdc. At 4Adc the drop is approximately 0.4Vdc. These values, other than the J3,3 RPC, are consistent with the 28Vdc RPCs (they are the same hybrids, after

all). However, because the voltage drop across the FET is current dependent, the percentage losses at the higher input values are 0.12% and 0.34%, respectively.

Bus A [V]	0			
Bus B [V]	120.2			
FRPC [Jx,n] or [m]	J22,1	J22,2	J22,3	J22,4
Load Current [A]	2.106	2.105	2.095	2.102
Vsense (POR) [V]	28.771	28.769	28.773	28.771
FRPC Vout [V]	28.58	28.57	28.58	28.59
Measured Drop [V]	0.192	0.198	0.19	0.185
Calculated Drop [V]	0.191	0.199	0.193	0.181
FRPC [Jx,n] or [m]	J22,1	J22,2	J22,3	J22,4
Load Current [A]	4.141	4.139	4.139	4.138
Vsense (POR) [V]	28.77	28.769	28.769	28.769
FRPC Vout [V]	28.35	28.33	28.36	28.4
Measured Drop [V]	0.42	0.436	0.408	0.371
Calculated Drop [V]	0.42	0.439	0.409	0.369

28Vdc Hybrid RPC voltage Drops
Table 1

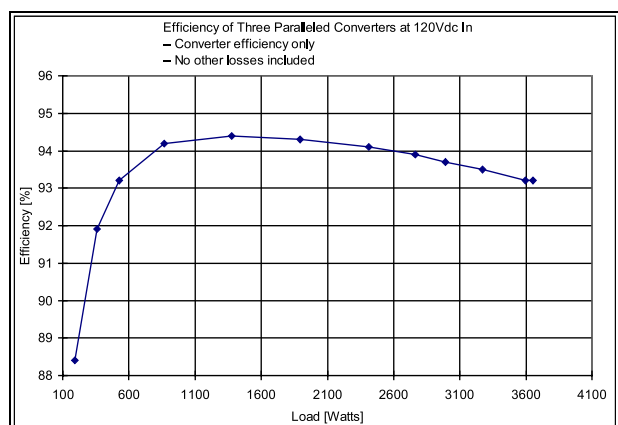
PROGRAMMING PINS & INITIAL POSITION

The control software developed for the EM EPCU, in conjunction with the “parallelable” loads of the HyberLoad load bank, afforded testing of the EPCU *Initial Position* (IP) and parallelability of EPCU 28Vdc channels. 120Vdc channels were similarly tested, using dip switches on a specially designed test harness.

The control software and HyberLoad combination eliminated the need to construct varying harnesses for different IP and paralleled channel scenarios, because the HyberLoads can “short” the appropriate pins within a harness. In this manner, all channels were verified to implement IP and paralleling properly.

EFFICIENCY of THREE PARALLELED PCUs

The efficiency of the PCUs were tested individually and with the three units paralleled. The efficiency numbers do not include the losses associated with the input RPC cards; however, the minimal losses associated with approximately 8 inches of #14 wires connecting the PCU outputs to the POR are included.



Efficiency of Paralleled Converters Only
Figure 1

The efficiency is over 93% for loads in the range of 500We to 3000We, and greater than 94% in the range of 800We to 2500We. The peak efficiency of the paralleled PCUs is approximately 94.4%. See Figure 1.

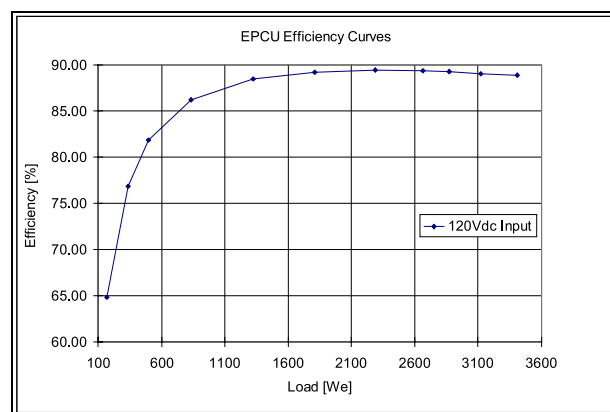
EPCU EFFICIENCY TESTS

The EPCU efficiency tests were run in two different modes of operation:

1. The EPCU having only 28Vdc loads connected. This mode's efficiency is referred to as the EPCU “converted-power efficiency” and includes all losses (e.g., A5 cards and housekeeping power requirements).
2. The EPCU having 28Vdc and 120Vdc loads connected. This efficiency is referred to as the “overall” or “box” efficiency.

The converted-power efficiency tests were run by connecting a 120Vdc power supply to each EPCU input bus, connecting two converters to Bus A, connecting one converter to Bus B, and measuring the input current and voltage at the input connectors; furthermore, a special harness was used to measure the total 28Vdc load current and the voltage at the output of one of the load RPCs (A5 cards). This test configuration results in a very good approximation of the converted-power efficiency, and is shown in Figure 2. The peak, converted-power efficiency is approximately 89.5%.

The design requirement for EPCU efficiency is defined for the overall efficiency, and is greater than 97% over the “midband” range of loads.



Converted Power Efficiency of EPCU
Figure 2

EPCU REGULATION, CURRENT-LIMITING, & FOLDBACK

The POR regulation with the three PCUs paralleled and connected to Bus B was tested at input voltages of 116Vdc, 120Vdc, and 126Vdc. The load was varied from 0% to 100% and it was found that the EPCU regulates the bus to within 0.17Vdc over the rated load range.

Voltage foldback occurs because the PWM controller cannot maintain a long enough duty cycle to regulate the POR voltage for a given load and input voltage. Thus, as the load increases, the input-voltage foldback point increases. The voltage foldback point, listed as V_{in} [V] in Table 2, for various load levels was found by decreasing the power supply voltage from 120Vdc until foldback occurred.

Load [A]	Load [We]	Vout [V]	Vin [V]
12	338	27.92	101.27
53.5	1500	28.04	104.71
107	3000	27.997	106.89

Input Voltage Foldback @ Three Load Levels
Table 2

SYSTEM & EPCU STABILITY TESTS

The EPCU was tested for large and small signal stability, as well as for stand-alone stability. *Small Signal Stability* (SmSS) is determined using the Nyquist stability criterion and Bode plots. Characterizing the response of the EPCU input and output to load-steps tested *Large Signal Stability* (LSS). A last measure of stability is the stand-alone stability, which is a special case of small signal stability.

LARGE SIGNAL STABILITY

Instead of using a power supply and a *Line Impedance Simulation Network* (LISN), these tests were performed by connecting the EPCU to the ISS power system test-bed located at GRC. A *Rocketdyne* (RKD) DDCU (rated at 6kWe) was connected to a Type III equivalent *Remote Power Control Module* (RPCM), which fed one input bus of the EPCU via 73feet of a #4 power line. Because the RKD DDCU is an EM unit and because the test setup mimics an ISS channel, the response of the system (i.e., EPCU, RPCM and DDCU) to a load step should be more indicative of what would occur on ISS.

LSS testing was accomplished by applying various load steps to the EPCU and monitoring the input and output transient responses. Of primary concern to the ISS EPS is the input response of the EPCU, which must not cause potential instabilities of the secondary power distribution system which lead to, for example, nuisance trips of RPCMs.

The worst-case test was the application of a 3kWe @28Vdc load-step (i.e., a 0%-to-100%) to an unloaded EPCU, having all three converters connected to one bus. The EPCU input-current response (Figure 3) demonstrates a time to first peak, T_p , of approximately 1.2msec., an input-current overshoot of approximately 55.7% (implies a damping ratio, ζ , of 0.183), and a settling time, T_s , of approximately 3.7msec. The input voltage (Figure 3) reaches a minimum of 119.6Vdc in approximately 900msec (undershoot is approximately 1.65% with a $\zeta = 0.793$), and the voltage T_s is undefined because it never exceeds 2% of its final value: That is, the input bus remains "stiff" in the presence of a large

load step placed on the EPCU. Thus, with a worst case load application, the EPCU settles to an input current value of 27Adc within 4msec of the load step, and—it can be concluded—it will not introduce instability on the input EPS.

Not shown is the EPCU output voltage response to the 0%-to-100% load step in which V_{out} reaches a minimum value of approximately 25.6Vdc 230 μ sec after the load step, and it recovers to within 2% of 28Vdc approximately 800 μ sec after the load step.

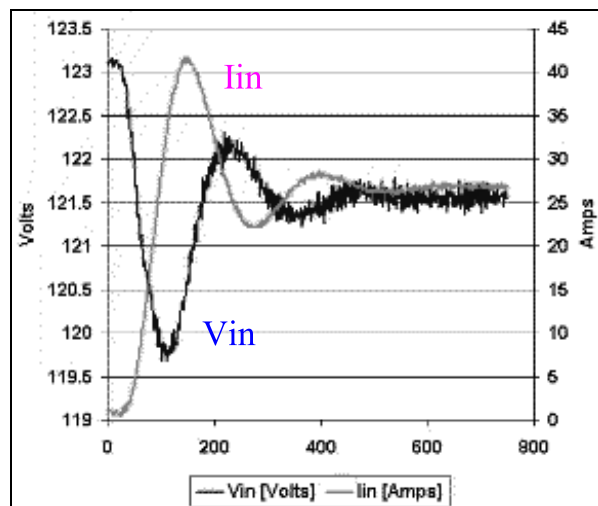


Figure 3

SMALL SIGNAL STABILITY TEST PROCEDURE & DEFINITION

SmSS testing was done using the Venable Systems' *Impedance Measurement System* (IMS). The IMS system injects a swept-frequency small AC signal (either voltage or current), and this small signal excitation and the corresponding response signals are used to determine the impedance of the system under test. For system stability tests, the source impedance (Z_{source}) seen by the EPCU input includes the DDCU output impedance, the power line, and intermediate switchgear. The load impedance (Z_{load}) is defined as the input impedance of the EPCU.

SmSS of the system is quantified in two ways. First, the Nyquist criterion absolutely ensures stability if and only if the contour of Z_{source}/Z_{load} does not encircle the $[-1, 0]$ point. Alternatively, an ISS requirement for stability imposed upon payloads is that the input impedance of the payload (i.e., the EPCU) falls within the prescribed magnitude and phase limits. The following sections describe the application of these stability requirements to the EPCU.

ISS REQUIREMENTS FOR SMALL SIGNAL STABILITY

The ISS payload stability requirements (SSP-57000) mandate that the magnitude of the load impedance shall not be lower than that of the source. If, however, the magnitude of the input impedance of the load is lower than that of the source, then the system will be stable if the phase of the load is bounded by the required limits.

Again, the EPCU was connected to the RKD DDCU and the IMS was used for SmSS testing.

The ISS impedance limit requirements and the small signal impedance of the EPCU, feeding a 107Adc load, are shown in Figure 4a. This Bode plot indicates that for frequencies below 300Hz, the magnitude of the EPCU input impedance is below the required limit. However, because its phase is within the required limits for frequencies less than 300Hz, the ISS requirements are met. Furthermore, the Nyquist plot (Figure 4b) demonstrates that the distribution system is unconditionally stable with the EPCU installed.

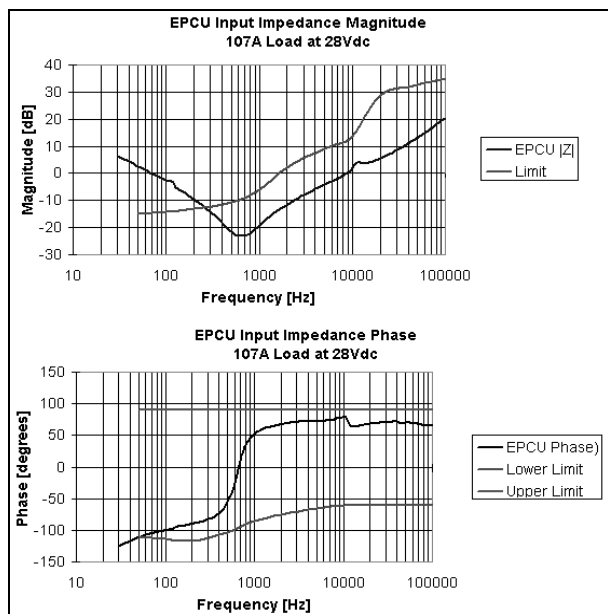


Figure 4a

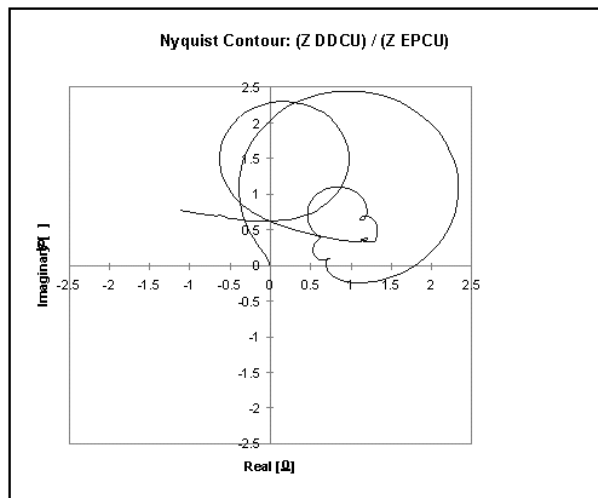


Figure 4b

STAND-ALONE STABILITY

Stand-alone stability was tested using the IMS with the EPCU connected to the RKD DDCU, as discussed above. The EPCU was tested under the following 28Vdc loads: 12Adc, 27Adc, 54Adc, 81Adc, and 105Adc. Opening the voltage feedback control loop of the EPCU, injecting a swept-frequency small signal AC stimulus into the voltage-control feedback loop, and then measuring the EPCU output response determines the stand-alone stability for each load condition. The loop gain (i.e., EPCU output response divided by the injected signal) of the EPCU was calculated and displayed by the IMS as both a Nyquist plot and Bode Plot.

The test results for the 105Adc load condition, using Nyquist's criteria and Bode diagrams, indicate that the EPCU is unconditionally stable, and that the EPCU has a stand-alone "gain margin" (i.e., impedance magnitude) of 15[dBΩ] and a minimum phase margin of 84[degrees]. The results for all aforementioned load conditions indicate that the EPCU should not cause the ISS power system to oscillate or become unstable.

LOAD SHARING

The EPCU is designed so that the active PCUs share load demand equally (i.e., 33% each, if three PCUs are active; 50% each, if two PCUs are active; 100% if only one PCU is active). This equal power share at the converter outputs results in unequal sharing of power by the 120Vdc input busses, if an unequal number of converters are connected to the input busses.

Consider the response of the EPCU to a slowly increasing load with two PCUs on one bus and the other PCU on the other bus: As the load demand increases, unequal sharing at the input continues until an allocation limit is reached; further increases in load are then met by drawing the required power from the bus still operating within its allocation limit. When both allocation limits are equaled, further increases in load will result in prioritized load shedding.

One dynamic response test of the load share control circuit was done by loading the EPCU to 1kWe, connecting one PCU to Bus A, and connecting two PCUs to Bus B. Bus A allocation was set to 460We and bus B to 8190We. A 28Vdc-load step of 1kWe was then applied and the response was captured with an oscilloscope. The scope traces are shown in Figure 5. (The scope was set in AC-coupled mode at 100mV/div to measure the bus voltage, and the scope was DC-coupled and set at 2.5A/div to measure each bus current.)

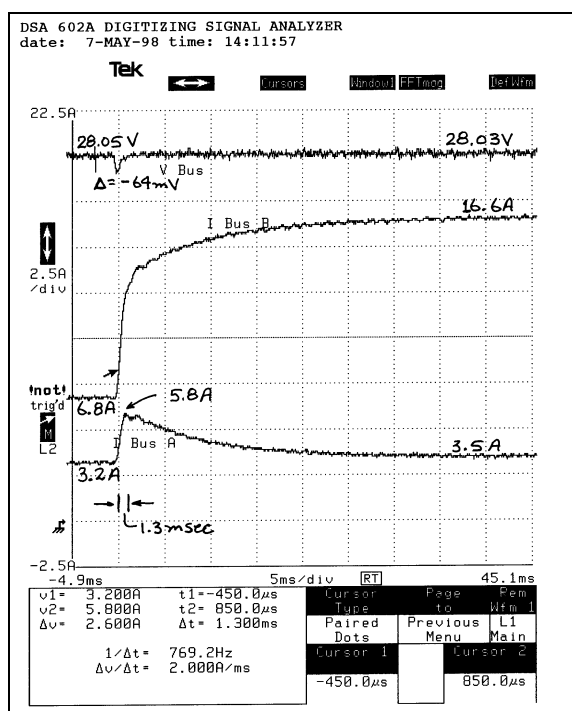


Figure 5

As can be seen in the traces, the busses share power in an approximately 2-to-1 fashion (i.e., 3.2Adc and 6.8Adc) prior to the allocation change. The introduction of the load step causes each bus to attempt to proportionally share the additional demand (i.e., the slope of the current response for Bus B is twice that of Bus A). However, because the allocation of Bus A is 460We, the DPS controller begins to limit the current after 1.3msec. The peak Bus A current is 5.8Adc. In steady state, Bus A is limited to 418We and Bus B picks up the remainder of the load. Also, note that the POR has an -64mV transient lasting approximately 500 μ sec.

RPC TRIP CHARACTERIZATION

The hybrids used on both the 120Vdc RPC cards (i.e., A12 and A13) and 28Vdc RPC cards (i.e., A5) are the same. The trip time of the hybrid is a v^2t relationship: that is, the higher the voltage drop across the hybrid's FET, the faster (exponentially) the FET is tripped off. A number of test conditions were run for the A5 cards to demonstrate the tripping of the RPC.

Characterization of the RPC trip curve was accomplished by turning the hybrid on into a short with varying input voltages. Because the FET voltage drop is typically 0.2Vdc under normally operating conditions, the FET voltage drop progressively increases beyond this

value as the hybrid goes "deeper" into current limit. Thus, by connecting a power supply directly to the input of the hybrid and turning the hybrid on into a short-circuit, the power supply voltage is equal to the FET voltage--thereby simulating various overload conditions. The trip curve is shown in Figure 6.

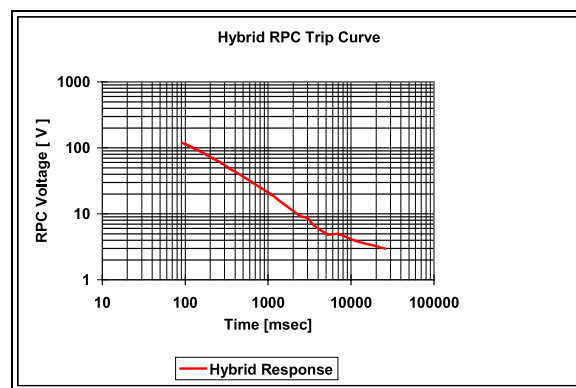


Figure 6

PRIORITIZED LOAD SHEDDING

PLS is an automatic means of ensuring that the most critical loads remain serviced, in the event that the DPS function cannot redistribute the load between the two input busses such that the feeds remain within their respective allocation limits. The load-shed control is a slower loop than the load share loop, which ensures that re-allocation of load (i.e., the DPS function) occurs first.

There are 16 levels of priority, including a "never shed" priority. PLS was tested under a variety of initial conditions (including one converter just entering current-limit mode) and with various transients (e.g., loss of an input bus).

Consider the PLS test for which the priority level of 16 4Adc channels was set at 16 successive levels, and the allocation of the busses was adjusted such that the total load on each was just equaled. (One PCU was connected to one bus and two PCUs to the other). A bulk load was then turned on. The total output current was measured by using a specially designed test-harness and the oscilloscope was set to trigger on the falling edge of the output current. Because the DPS controls could not redistribute the load without exceeding both bus allocations, loads were shed. Figure 7 is an oscilloscope-captured output-current transient response of the load shedding function. (Because of insufficient bulk load, the response indicates only 13 load-shed steps.) Notice that the load shedding of 13 load levels occurred within 1sec and that the POR voltage does not show any significant transient.

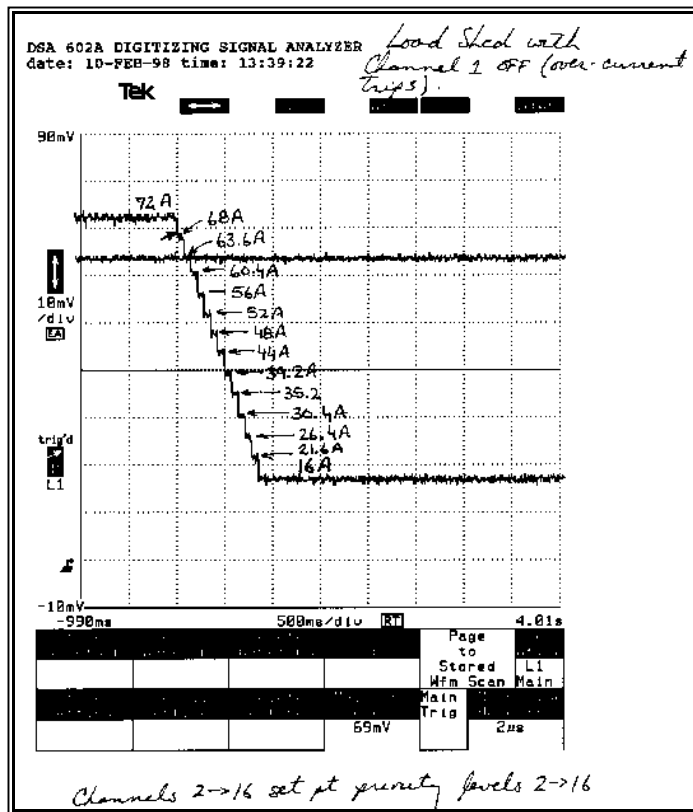


Figure 7

THERMAL-VACUUM TEST

Although the EPCU will be used in a pressurized module, it was tested in a thermal-vacuum chamber. (The rationale being that an experiment may be required to continue in the event that depressurization occurs and may not be sensed quickly enough to command off the EPCU.) A total of 44 thermocouples were mounted on and within the EPCU at points deemed critical to EPCU operation.

The EPCU will be connected to the ISS *Thermal Management System* (TMS) via two "quick disconnects" on the back of the unit. Coolant flows through a serpentine path within the base-plate of the EPCU. (The Space Station thermal system coolant specifications are 40[lbs./Hr] @ 65F and 200[lbs./Hr] @ 115F.)

Thirty-two thermal data points were electronically collected by a Molytec data acquisition system and sent to a PC; the remaining 12 channels were collected with an external data acquisition system and also sent to the PC. Three of the data points are external temperature measurements—most notably the faceplate temperature, which is important because the "touch temperature" is required to be below 114F.

Initial testing of the EPCU was done in open-air conditions at various load levels (i.e., 50% and 100% rated load levels) to obtain a baseline of performance. Furthermore, these baseline tests were performed with maximum cooling to establish the baseline data with low

risk to the unit. The tests were then repeated in vacuum and the thermal rejection and operating temperatures were measured.

The thermal-vacuum tests highlighted a number of problems, which were corrected. These included the PCB-to-card guide and the RPC-to-PCB interfaces, which resulted in operating temperatures (in vacuum) higher than acceptable. These interfaces were corrected with the application of Cotherm, and the RPC-hybrid operating temperatures have been reduced by 30F—back to within acceptable levels.

ELECTRO-MAGNETIC INTERFERENCE TESTS

The *Engineering Model* (EM) EPCU was tested according to the *International Space Station* (ISS) Electromagnetic Emissions and Susceptibility Requirements (documents SSP 30237 rev C and SSP30238 rev C). The tests were conducted in the NASA GRC's EMI Laboratory. These tests involved conducted emissions tests on the EPCU input and output power terminals, conducted power line DC transients, conducted susceptibility, radiated emissions, and radiated susceptibility.

Additional tests were run from the ISS Pressurized Payloads Interface Requirements Document (SSP 57000). These additional tests involved EPCU output voltage ripple frequency spectrum, time domain input voltage ripple measurements, large signal stability tests, and common mode voltage and current susceptibility tests.

The unit passed most EMI tests necessary for ISS flight qualification. Those it did not pass were either corrected or shall have waivers sought. EMI test procedures and test results are fully documented in the Fluids and Combustion Facility EPCU EM EMI Test Report.

VIBRATION TESTS

The EM EPCU was not originally intended to undergo vibration tests, because many of its integrated circuit and electronic components are mounted in sockets. However, the Electrical Systems Development Branch decided to run vibration tests with the EM unit to verify the structural design of the unit, and to identify major structural problems that would require a major redesign of the EPCU. The vibration tests were run in NASA GRC's Structural Dynamics Lab. Vibration tests included 2.5 minutes of 20 to 2000 Hz random vibration on the x, y, and z axes at a level of 4.4 g's RMS and 7.4 g's RMS. Also, there was a sine burst test of 30 cycles at 20 Hz along the x-axis. This test was intended to simulate impulse acceleration in the direction of the flight. The levels for this sine burst test were 7 g's RMS and 14.8 g's RMS for 1.5 seconds. Sine wave characterization sweep tests from 20 to 500 Hz (2 octave/minute) at 0.25g's were run before and after each vibration test in order to detect any abnormal resonance that would indicate any damage to the unit during the test.

In addition, electrical checkout tests were run on the EPCU after each vibration test to make sure that the unit was still fully operational. The EPCU EM passed the qualification level vibration tests required for space shuttle launch and ISS flight. The vibration test profiles and EPCU accelerometers data are fully documented in the Fluids and Combustion Facility EPCU EM Vibration Test Report.

CONCLUSIONS

The Engineering Model Electrical Power Control Unit is a 3kWe power interface designed to interface 28Vdc Fluids/Combustion Facility Experiments with the International Space Station's 120Vdc-distribution bus. The EPCU incorporates Dynamic Power Sharing and Prioritized Load Shedding to effectively utilize allocated power and to ensure sustained power for critical loads during abnormal operating conditions.

Initial testing of the EM EPCU was completed in October 1998. The EPCU passed the electrical, thermal, EMI, and thermal/vacuum tests, which identified only a few correctable problems.

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